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September 15, 2017
STEELDAY
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September 15, 2017
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Course Description

Designing in Structural Steel: 2017

September 15, 2017

This webinar highlights the most significant changes in the 2016 AISC *Specification for Structural Steel Buildings* and *Code of Standard Practice* as well as the 15th Edition *Steel Construction Manual*.

Topics include:

- Member design for tension and compression
- Connection design
- New material standards and steel shapes
- New Super Table for members subject to axial, shear, flexure and combined forces
- Inclusion of digital models in contract documents
- New and improved provisions for architecturally exposed structural steel



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Learning Objectives

- Identify key changes to the AISC *Specification*
- Identify key changes to the AISC *Code of Standard Practice*
- Identify key changes to the AISC *Steel Construction Manual*
- Locate additional AISC resources including additional steel section properties and design examples



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Designing in Structural Steel: 2017



Larry Kruth, PE
Vice President of Engineering and Research
AISC
Chicago, IL


There's always a solution in steel.



AISC 15th Edition Steel Construction Manual

*Specification for Structural Steel Buildings
&
Code of Standard Practice for Steel Buildings and Bridges*

Lawrence F. Kruth, PE

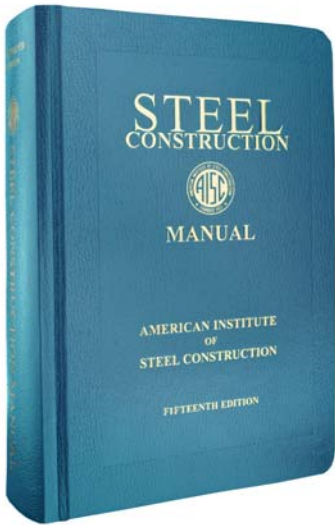


September 15, 2017





15th Edition
AISC Steel Construction Manual



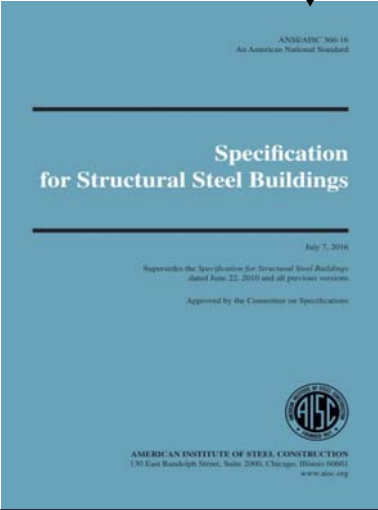
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2016 AISC Standards



2018 *INTERNATIONAL BUILDING CODE*



2016 AISC Standards



AISC
Specification for Structural
Steel Buildings
(ANSI/AISC 360-16)



2016 AISC Standards: AISC 360-16



Specification for Structural Steel Buildings

- Chapter A. General Provisions
- Chapter B. Design Requirements
- Chapter C. Design for Stability
- Chapter D. Design of Members for Tension
- Chapter E. Design of Members for Compression
- Chapter F. Design of Members for Flexure
- Chapter G. Design of Members for Shear
- Chapter H. Design of Members for Combined Forces and Torsion

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2016 AISC Standards: AISC 360-16



Specification for Structural Steel Buildings

- Chapter I. Design of Composite Members
- Chapter J. Design of Connections
- Chapter K. ~~Design of HSS and Box Members Connections~~ Additional Requirements for HSS and Box-Section Connections**
- Chapter L. Design for Serviceability
- Chapter M. Fabrication and Erection
- Chapter N. Quality Control and Quality Assurance

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2016 AISC Standards: AISC 360-16



Specification for Structural Steel Buildings

Appendix 1. Design by ~~Inelastic~~ Advanced Analysis

Appendix 2. Design for Ponding

Appendix 3. ~~Design for~~ Fatigue

Appendix 4. Structural Design for Fire Conditions

Appendix 5. Evaluation of Existing Structures

Appendix 6. Member Stability Bracing for ~~Columns and Beams~~

Appendix 7. Alternative Methods of Design for Stability

Appendix 8. Approximate Second-Order Analysis

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2016 AISC Standards: AISC 360-16



Section A2

REFERENCED SPECIFICATIONS, CODES AND STANDARDS

New Referenced Standards:

- 2016 ASCE 7
- 2015 AWS D1.1
- 2014 RCSC Specification
- 2014 ACI 318

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2016 AISC Standards: AISC 360-16



Section A2

REFERENCED SPECIFICATIONS, CODES AND STANDARDS

New HSS Standards:

- **ASTM 1065 – New HSS material**
- **ASTM 1085 – New HSS material**

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2016 AISC Standards: AISC 360-16



Section A2

REFERENCED SPECIFICATIONS, CODES AND STANDARDS

ASTM F3125 – New bolt standard

Encompasses Grades:

A325, A325M, A490, A490M,

F1852 & F2280

ASTM F3043 – 200 ksi TC bolt

ASTM F3111 – 200 ksi heavy hex bolt

AWS A5.36 – Flux cored & metal cored electrodes

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Chapter D

DESIGN OF MEMBERS FOR TENSION

Revision to Table D3.1, Shear Lag Factors, *U*

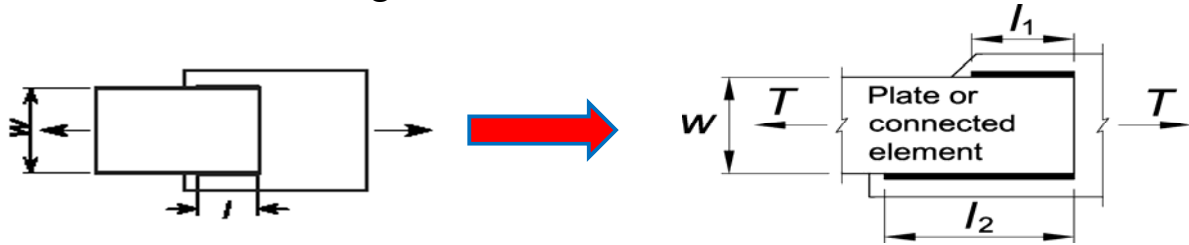
2016 AISC Standards: AISC 360-16



TABLE D3.1

Shear Lag Factors for Connections to
Tension Members

U = shear lag factor from Table D3.1, Case 4



2010

2016



2016 AISC Standards: AISC 360-16



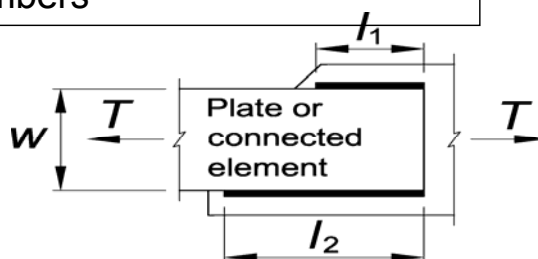
TABLE D3.1

Shear Lag Factors for Connections to Tension Members

Revised Case 4:

$$U = \left(\frac{3l^2}{3l^2 + w^2} \right) \left(1 - \frac{\bar{x}}{l} \right)$$

where $l = \frac{l_1 + l_2}{2} \geq 4 \times (\text{weld size})$



P. Fortney & W. Thornton,
AISC Engineering Journal, 2012

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Chapter E

DESIGN OF MEMBERS FOR COMPRESSION

- ***KL, effective length* → L_c**
- **Slender element members:**
revised procedure → no more Q factor

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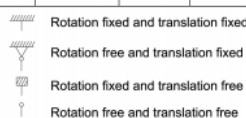
L_c Replaces K-Factor



- *K*-factor
 - First introduced in the 1963 Specification
 - Set equal to 1.0 when using the direct analysis method of Chapter C (since 2005)
 - For 2016, *KL*, the effective length, has been replaced with *L_c*. This makes the designation of effective length simpler since in some instances, such as for torsion, the traditional definition of *K* is not helpful.
 - This has been implemented throughout the 2016 Specification

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TABLE C-A-7.1 Approximate Values of Effective Length Factor, <i>K</i>						
	(a)	(b)	(c)	(d)	(e)	(f)
Buckled shape of column is shown by dashed line						
Theoretical <i>K</i> value	0.5	0.7	1.0	1.0	2.0	2.0
Recommended design value when ideal conditions are approximated	0.65	0.80	1.2	1.0	2.1	2.0
End condition code						



2016 AISC Standards: AISC 360-16



Chapter J

DESIGN OF CONNECTIONS

- ☐ Bolts in Combination with Welds (Sect. J1.8)
- ☐ New ASTM bolt standards (Sect. J3)
- ☐ New Group C bolts (Sect. J3)

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2016 AISC Standards: AISC 360-16



Section J3

BOLTS AND THREADED PARTS

- New high-strength bolt spec: ASTM F3125
Group A: **ASTM F3125 Grades** A325, A325M, F1852 and ASTM A354 Grade BC
Group B: **ASTM F3125 Grades** A490, A490M, F2280 and ASTM A354 Grade BD
Group C: ASTM F3043 and F3111

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Chapter J

DESIGN OF CONNECTIONS

- ☐ Increase in pretension for bolts (Sect. J3)
- ☐ Change in minimum bolt hole size (Sect. J3)

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2016 AISC Standards: AISC 360-16



Section J3

BOLTS AND THREADED PARTS

- Table J3.1: Increased min. bolt pretension for Group A bolts for $d_b \geq 1 \frac{1}{8}$ in.
- Table J3.3: Nominal hole sizes of std., SS & LS width when ≥ 1 in. → increase to 1/8 in. oversize

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2016 AISC Standards: AISC 360-16



Chapter J

DESIGN OF CONNECTIONS

- ☐ New minimum bolt hole clear spacing, d (Sect. J3.3)
- ☐ Revised presentation of bearing and tearout equations (Sect. J3.10)
- ☐ Incorporated HSS connections into Sect. J10
- ☐ Washer requirements moved to RCSC

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2016 AISC Standards



AISC *Code of Standard Practice for Steel Buildings and Bridges* (ANSI/AISC 303-16)

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2016 AISC Standards: AISC 303-16



Code of Standard Practice **ANSI/AISC 303-16**

Balanced committee

- Fabricators - 7
- Engineers - 7
- Others – 9
 - General Contractor
 - Code Official
 - Quality Consultant
 - Erector
 - Detailer
 - Architect
 - Attorney

Rigorous public review process

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2016 AISC Standards: AISC 303-16



Code of Standard Practice for Steel Buildings and Bridges

1. General Provisions
 2. Classification of Materials
 3. **Design Documents** ~~Drawings~~ and Specifications
 4. **Approval Documents** ~~Shop and Erection Drawings~~
 5. Materials
 6. Shop Fabrication and Delivery
 7. Erection
 8. Quality Control
 9. Contracts
 10. Architecturally Exposed Structural Steel
- ~~Appendix A. Digital building Product Models~~

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2016 AISC Standards: AISC 303-16



Code of Standard Practice

Three Major Revisions in 2016

- 1: Models**
- 2: Stiffening**
- 3: Architectural Exposed Structural Steel (AESS)**

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2016 AISC Standards: AISC 303-16



Code of Standard Practice

1: Models

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2016 AISC Standards: AISC 303-16



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2016 AISC Standards: AISC 303-16



1: Models

~~2010—design drawings~~

2016 – **design documents**

- **design documents.** The *design drawings*, or where the parties have agreed in the *contract documents* to provide digital model(s), the *design model*. A combination of drawings and digital models also may be provided.
- **design model.** A dimensionally accurate 3D digital model of the structure that conveys the *structural steel* requirements given in Section 3.1 for the building.

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2016 AISC Standards: AISC 303-16



1: Models

~~2010—shop drawings~~

2016-**fabrication documents**

- **fabrication documents.** The *shop drawings*, or where the parties have agreed in the *contract documents* to provide digital model(s), the *fabrication model*. A combination of drawings and digital models also may be provided.
- **fabrication model.** A dimensionally accurate 3D digital model produced to convey the information necessary to fabricate the *structural steel*. This may be the same digital model as the *erection model*, but it is not required to be.

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2016 AISC Standards: AISC 303-16



1: Models

~~2010—erection drawings~~

2016-erection documents

- **erection documents.** The *erection drawings*, or where the parties have agreed in the *contract documents* to provide digital model(s), the *erection model*. A combination of drawings and digital models also may be provided.
- **erection model.** A dimensionally accurate 3D digital model produced to convey the information necessary to erect the structural steel. This may be the same digital model as the *fabrication model*, but it is not required to be.

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2016 AISC Standards: AISC 303-16



1: Models

~~2010—shop and erection drawings~~

2016- approval documents

- **approval documents.** The *structural steel shop drawings*, *erection drawings*, and *embedment drawings*, or where the parties have agreed in the *contract documents* to provide digital model(s), the *fabrication and erection models*. A combination of drawings and digital models also may be provided.

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2016 AISC Standards: AISC 303-16



2: Stiffening

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2016 AISC Standards: AISC 303-16



2: Stiffening

2010

Section 3.1.1: Column stiffeners, bearing stiffeners, doublers, etc., must be designed and clearly shown on drawings

Section 3.1.2: Three options for connection design indicated by owner's designated rep. for design (ODRD)

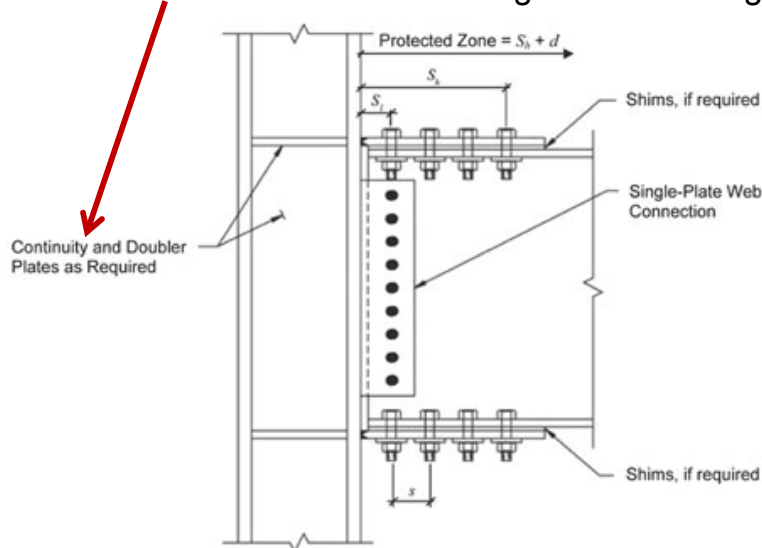
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Often missed in connection design when bidding



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2016 AISC Standards: AISC 303-16



2016

Section 3.1.1

Connection Design Responsibility

Option 1:

ODRD (EOR) provides complete connection design

Option 2:

Steel detailer selects or completes connection design

Option 3:

Licensed engineer working for fabricator provides complete connection design

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2016 AISC Standards: AISC 303-16



2016

Section 3.1.2 Connection Stiffening

If Option 1 or 2, ODRD designs stiffening and shows on structural design bid documents

If Option 3A, ODRD designs stiffening and shows on structural design bid documents

If Option 3B, ODRD provides bidding quantity of items for stiffening (an estimate). If no estimate provided, stiffening will not be included in bid.

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3: Architecturally Exposed Structural Steel (AESS)

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2016 AISC Standards: AISC 303-16



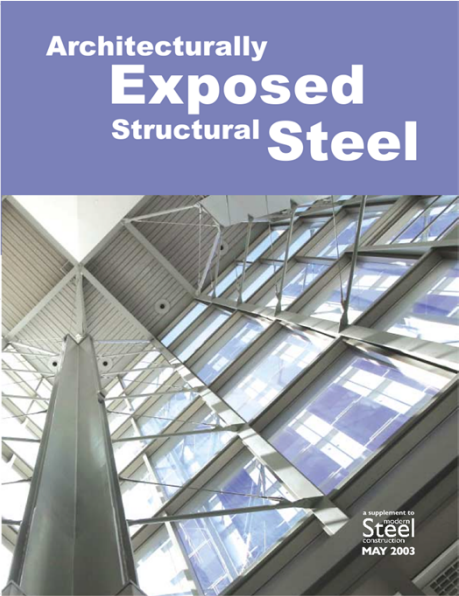
3: AESS

Section 10 completely changed

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2016 AISC Standards: AISC 303-16



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2016 AISC Standards: AISC 303-16



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2016 AISC Standards: AISC 303-16



3: AESS

Section 10 completely changed

- AESS 1: Basic elements
- AESS 2: Feature elements > 20 ft
- AESS 3: Feature elements ≤ 20 ft
- AESS 4: Showcase elements w/special surface & edge treatment
- AESS C: Custom

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2016 AISC Standards: AISC 303-16



3: AESS

Section 10 completely changed

- AESS 1: \$
- AESS 2: \$\$
- AESS 3: \$\$\$
- AESS 4: \$\$\$\$
- AESS C: \$\$\$\$\$

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2016 AISC Standards: AISC 303-16



Some Additional Revisions:

- Lack of tolerances
- Identifying protected zones
- Handling cost of revisions
- Anchor rod placement tolerances

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2016 AISC Standards: AISC 303-16



Section 1.10

No zero tolerance.

1.10. Tolerances

Tolerances for materials, fabrication and erection shall be as stipulated in Sections 5, 6, 7, and 10. Tolerances absent from this Code or the contract documents shall not be considered zero by default.

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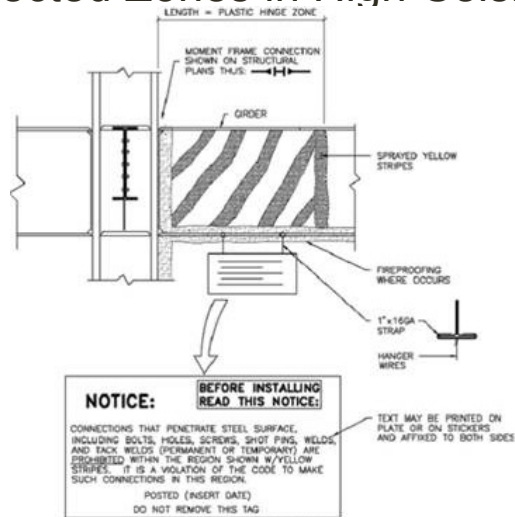


2016 AISC Standards: AISC 303-16



Section 1.11

Marking of Protected Zones in High-Seismic Applications



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2016 AISC Standards: AISC 303-16



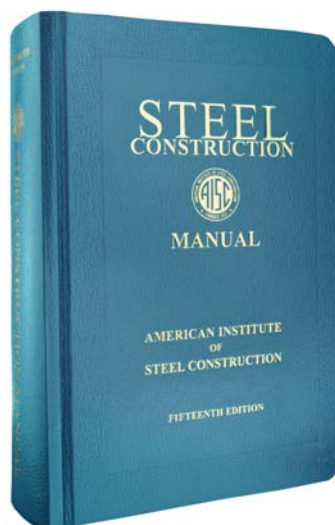
Section 7.5.1

Tolerances for anchor-rod placement have been revised for consistency with the hole sizes provided in the *AISC Manual* and tolerances given in ACI 117.

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15th Edition AISC Steel Construction Manual



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- Part 1. Dimensions and Properties
- Part 2. General Design Considerations
- Part 3. Design of Flexural Members
- Part 4. Design of Compression Members
- Part 5. Design of Tension Members
- Part 6. Design of Members Subject to Combined Forces
- Part 7. Design Considerations for Bolts
- Part 8. Design Considerations for Welds
- Part 9. Design of Connecting Elements

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- Part 10. Design of Simple Shear Connections
- Part 11. Design of Partially Restrained Moment Connections
- Part 12. Design of Fully Restrained Moment Connections
- Part 13. Design of Bracing Connections and Truss Connections
- Part 14. Design of Beam Bearing Plates, Column Base Plates,
Anchor Rods and Column Splices
- Part 15. Design of Hanger Connections, Bracket Plates, and
Crane-Rail Connections

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- Part 16. Standards
 - 2016 AISC *Specification for Structural Steel Buildings*
 - 2014 RCSC *Specification for Structural Joints Using High-Strength Bolts*
 - 2016 AISC *Code of Standard Practice for Steel Buildings & Bridges*

Part 17. Misc. Data and Mathematical Information

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Part 1. Dimensions and Properties



- New shapes:
 - W-shapes (& corresponding WT-shapes)
 - HP-shape
 - Angles
 - HSS
 - Pipe

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Part 1. Dimensions and Properties



W-Shapes
W40x655
W36x925
W36x853
W36x802
W36x723
W21x275
W21x248
W21x223
W14x873
W14x808



HP-Shapes
HP12x89



Angles
L12x12x1-3/8
L12x12x1-1/4
L12x12x1-1/8
L12x12x1
L10x10x1-3/8
L10x10x1-1/4
L10x10x1-1/8
L10x10x1
L10x10x7/8
L10x10x3/4

& corresponding WT-shapes

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Part 1. Dimensions and Properties



HSS22x22x7/8, 3/4
HSS20x20x7/8, 3/4, 5/8, 1/2
HSS18x18x7/8, 3/4, 5/8, 1/2
HSS16x16x7/8, 3/4
HSS14x14x7/8, 3/4
HSS16x16x7/8, 3/4
HSS14x14x7/8, 3/4
HSS12x12x3/4
HSS10x10x3/4



HSS24x12x3/4, 5/8, 1/2
HSS20x12x3/4
HSS16x12x3/4



Pipe 26, 24, 20, 18, 16, 14 (std and x-strong)
& Pipe 12, 10 (xx-strong)

Part 1. Dimensions and Properties



- New shapes
- Updated fillet radii $\longrightarrow k_{det}, k_1, T$ affected

Table 1-1
W-Shapes
Dimensions

Shape	Area, A	Depth, d	Web		Flange		Distance								
			Thickness, t _w	t _w 2	Width, b _f	Thickness, t _f	k								
							k _{det}	k _{det}	k ₁	T	Work- able Gage				
	in. ²	in.	in.	in.	in.	in.	in.	in.	in.	in.	in.				
W44x335 ^c	98.5	44.0	44	1.03	1	1/2	15.9	16	1.77	13/4	2.56	3	13/4	38	5 1/2
x290 ^c	85.4	43.6	43 3/8	0.865	7/8	7/16	15.8	15 7/8	1.58	19/16	2.36	2 13/16	1 9/8		
x262 ^c	77.2	43.3	43 1/4	0.785	13/16	7/16	15.8	15 3/4	1.42	17/16	2.20	2 5/8	1 9/8		
x230 ^c	67.8	42.9	42 7/8	0.710	11/16	3/8	15.8	15 3/4	1.22	1 1/4	2.01	2 1/16	1 9/16	↓	↓



Part 1. Dimensions and Properties

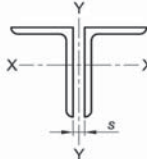


- New shapes
- Updated fillet radii $\longrightarrow k_{det}, k_1, T$ affected
- Larger separation for new double angles (2L12 and 2L10)

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Part 1. Dimensions and Properties



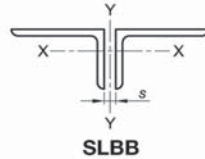


LLBB

Table 1-15

Double Angles

Properties



SLBB

Shape	Area, A	Radius of Gyration									
		LLBB				SLBB					
		r _y			r _x	r _y			r _x		
		Separation, s, in.				Separation, s, in.					
		0	3/4	1 1/2		0	3/4	1 1/2			
	in. ²	in.	in.	in.	in.	in.	in.	in.			
2L12×12×13/8	62.2	5.06	5.32	5.60	3.64	5.06	5.32	5.60	3.64		
×1 1/4	56.8	5.04	5.29	5.57	3.66	5.04	5.29	5.57	3.66		
×1 1/8	51.6	5.02	5.28	5.55	3.68	5.02	5.28	5.55	3.68		
×1	46.0	5.00	5.25	5.54	3.70	5.00	5.25	5.54	3.70		

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Part 2. General Design Considerations



- Table 2-4: Applicable ASTM Specifications for Various Structural Shapes
- Table 2-5: Applicable ASTM Specifications for Plates and Bars
- Table 2-7: Summary of Surface Preparation Standards

Part 2. General Design Considerations



Table 2-4
Applicable ASTM Specifications
for Various Structural Shapes

Steel Type	ASTM Designation		F _y Yield Stress ^a (ksi)	F _u Tensile Stress ^a (ksi)	Applicable Shape Series									
					W	M	S	HP	C	MC	L	HSS		
												Rect.	Round	Pipe
A500	A36		36	58–80 ^b										
	A53 Gr. B		35	60										
	Gr. B	42	58											
		46	58											
		46	62											
		50	62											
	Gr. A		36	58										



Part 2. General Design Considerations



Table 2-5
Applicable ASTM Specifications
for Plates and Bars

Steel Type	ASTM Designation	F _y Yield Stress ^a (ksi)	F _u Tensile Stress ^a (ksi)	Plates and Bars, in.									
				to 0.75 incl.	over 0.75 to 1.25 incl.	over 1.25 to 1.5 incl.	over 1.5 to 2 incl.	over 2 to 2.5 incl.	over 2.5 to 4 incl.	over 4 to 5 incl.	over 5 to 6 incl.	over 6 to 8 incl.	over 8
Carbon	A36	32	58-80										
		36	58-80										
	A283 ^a	Gr. C	30	55-75				d					
		Gr. D	33	60-80				d					
	A529	Gr. 50	50	65-100	b	b	b	b	b				
		Gr. 55	55	70-100	c	c	c	c	c				
	A709	Gr. 36	36	58-80									
Alloys	A572	Gr. 42	42	60									
		Gr. 50	50	65									
		Gr. 55	55	70									
		Gr. 60	60	75									
		Gr. 65	65	80									

Part 4. Design of Compression Members



- Eliminated *K* factor in tables/discussion → *L_c*
- Clarifies *C_w* = 0 is used in WT column tables
- Chapter E revisions reflected in tables
 - Slender members
 - Double angles use more general *F_{cr}* equation
- Removed Tables 4-13 to 4-20: Composite Columns
- W-shape column tables: added 65 and 70 ksi for some



Part 4. Design of Compression Members



- W-shape column tables: added 65 and 70 ksi for some

Table 4-1b

Available Strength in Axial Compression, kips

W-Shapes

$F_y = 65 \text{ ksi}$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

W14

Shape	W14x							
lb/ft	873 ^b		806 ^b		730 ^b		665 ^b	
Design	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD
0	10000	15000	9260	13900	8370	12600	7630	11500

Table 4-1c

Available Strength in Axial Compression, kips

W-Shapes

$F_y = 70 \text{ ksi}$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

W14

Shape	W14x							
lb/ft	873 ^b		806 ^b		730 ^b		665 ^b	
Design	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD
0	10800	16200	9980	15000	9010	13500	8220	12300

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The Super Table

Table 6-2

Available Strength for Members Subject to Axial, Shear, Flexural and Combined Forces

W-Shapes

$F_y = 50 \text{ ksi}$

$F_u = 65 \text{ ksi}$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

W44

Shape	W44x							
lb/ft	338 ^a		290 ^a		262 ^a		242 ^a	
Design	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD
0	4040	6060	3520	5280	3170	4760	2870	4300
1	4040	6060	3520	5280	3170	4760	2870	4300
2	4040	6060	3520	5280	3170	4760	2870	4300
3	4040	6060	3520	5280	3170	4760	2870	4300
4	4040	6060	3520	5280	3170	4760	2870	4300
5	4040	6060	3520	5280	3170	4760	2870	4300
6	4040	6060	3520	5280	3170	4760	2870	4300
7	4040	6060	3520	5280	3170	4760	2870	4300
8	4040	6060	3520	5280	3170	4760	2870	4300
9	4040	6060	3520	5280	3170	4760	2870	4300
10	4040	6060	3520	5280	3170	4760	2870	4300
11	4040	6060	3520	5280	3170	4760	2870	4300
12	4040	6060	3520	5280	3170	4760	2870	4300
13	4040	6060	3520	5280	3170	4760	2870	4300
14	4040	6060	3520	5280	3170	4760	2870	4300
15	4040	6060	3520	5280	3170	4760	2870	4300
16	4040	6060	3520	5280	3170	4760	2870	4300
17	4040	6060	3520	5280	3170	4760	2870	4300
18	4040	6060	3520	5280	3170	4760	2870	4300
19	4040	6060	3520	5280	3170	4760	2870	4300
20	4040	6060	3520	5280	3170	4760	2870	4300
21	4040	6060	3520	5280	3170	4760	2870	4300
22	4040	6060	3520	5280	3170	4760	2870	4300
23	4040	6060	3520	5280	3170	4760	2870	4300
24	4040	6060	3520	5280	3170	4760	2870	4300
25	4040	6060	3520	5280	3170	4760	2870	4300
26	4040	6060	3520	5280	3170	4760	2870	4300
27	4040	6060	3520	5280	3170	4760	2870	4300
28	4040	6060	3520	5280	3170	4760	2870	4300
29	4040	6060	3520	5280	3170	4760	2870	4300
30	4040	6060	3520	5280	3170	4760	2870	4300
31	4040	6060	3520	5280	3170	4760	2870	4300
32	4040	6060	3520	5280	3170	4760	2870	4300
33	4040	6060	3520	5280	3170	4760	2870	4300
34	4040	6060	3520	5280	3170	4760	2870	4300
35	4040	6060	3520	5280	3170	4760	2870	4300
36	4040	6060	3520	5280	3170	4760	2870	4300
37	4040	6060	3520	5280	3170	4760	2870	4300
38	4040	6060	3520	5280	3170	4760	2870	4300
39	4040	6060	3520	5280	3170	4760	2870	4300
40	4040	6060	3520	5280	3170	4760	2870	4300
41	4040	6060	3520	5280	3170	4760	2870	4300
42	4040	6060	3520	5280	3170	4760	2870	4300
43	4040	6060	3520	5280	3170	4760	2870	4300
44	4040	6060	3520	5280	3170	4760	2870	4300
45	4040	6060	3520	5280	3170	4760	2870	4300
46	4040	6060	3520	5280	3170	4760	2870	4300
47	4040	6060	3520	5280	3170	4760	2870	4300
48	4040	6060	3520	5280	3170	4760	2870	4300
49	4040	6060	3520	5280	3170	4760	2870	4300
50	4040	6060	3520	5280	3170	4760	2870	4300

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Example—Table 6-2



Given: W14x99, ASTM A992, pinned ends ($K = 1.0$),
 $L_{cx} = L_{cy} = L_b = 14$ ft
Check shape for combined loading using LRFD, with
required strengths as follows:

LRFD

$P_u = 400$ kips
 $M_{ux} = 250$ kip-ft
 $M_{uy} = 80.0$ kip-ft

Example— Table 6-2

Solution:

$\phi_c P_n = 1130$ kips

$\phi_b M_{nx} = 642$ kip-ft


Table 6-2 (continued)

Available Strength for Members

Subject to Axial, Shear,

Flexural and Combined Forces

W-Shapes



W14

$F_y = 50$ ksi

$F_u = 65$ ksi

109

99

90

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

P_n/Ω_c

$\phi_c P_n$

Available Compressive Strength, kips

ASD

LRFD

ASD

LRFD

ASD

LRFD

Shape

lb/ft

Design

W14x

109

99

90

M_{nx}/Ω_b

$\phi_b M_{nx}$

M_{nx}/Ω_b

$\phi_b M_{nx}$

M_{nx}/Ω_b

$\phi_b M_{nx}$

Available Flexural Strength, kip-ft

ASD

LRFD

ASD

LRFD

ASD

LRFD

923

1390

839

1260

764

1150

913

1370

830

1250

755

1140

901

1350

819

1230

745

1120

888

1340

807

1210

735

1100

874

1310

794

1190

723

1090

859

1290

780

1170

710

1070

843

1270

766

1150

697

1050

826

1240

750

1130

682

1030

808

1210

733

1100

667

1000

789

1190

716

1080

652

979

770

1160

698

1050

635

955

750

1130

680

1020

618

929

729

1100

661

994

601

903

708

1060

642

964

583

877

664

998

602

904

547

822

620

931

561

843

509

766

574

863

519

781

472

709

529

796

478

719

434

653

485

729

438

658

397

597

441

663

398

598

361

543

399

600

360

541

326

490

359

539

323

485

292

439

322

484

290

435

262

394

290

437

261

393

237

356

263

396

237

356

215

323

240

361

216

325

196

294

Effective length, L_e , ft, with respect to least radius of gyration, r_y , or unbraced length, L_b , ft, for X-X axis bending

8

479

720

430

646

382

574

9

479

720

430

646

382

574

10

479

720

430

646

382

574

11

479

720

430

646

382

574

12

479

720

430

646

382

574

13

479

720

430

646

382

574

14

475

714

427

642

382

574

15

470

706

422

635

382

574

16

465

699

417

627

378

568

17

460

691

413

620

373

560

18

455

684

408

613

368

553

19

450

676

403

605

363

546

20

445

669

398

598

358

539

22

435

654

388

583

349

524

24

425

639

378

569

339

510

26

415

623

369

554

329

495

28

405

608

359

539

320

481

30

395

593

349

524

310

466

32

385

578

339

510

300

452

34

375

563

329

495

291

437

36

365

548

320

480

281

423

38

355

533

310

466

271

408

40

345

518

300

451

262

394

42

335

503

290

436

252

379

44

325

488

280

422

239

359



Example—Table 6-2



Given: W14x99, ASTM A992, pinned ends ($K = 1.0$),
 $L_{cx} = L_{cy} = L_b = 14$ ft
Check shape for combined loading using LRFD, with
required strengths as follows:


LRFD

$P_u = 400$ kips
 $M_{ux} = 250$ kip-ft
 $M_{uy} = 80.0$ kip-ft

Example—Table 6-2



Solution:
 $\phi_b M_{ny} = 311$ kip-ft

Table 6-2 (continued) Available Strength for Members Subject to Axial, Shear, Flexural and Combined Forces W-Shapes												 W14
W14x						Shape lb/ft	W14x					
109							99 [†]					
P_n/Ω_c	$\phi_c P_n$	P_n/Ω_c	$\phi_c P_n$	P_n/Ω_c	$\phi_c P_n$	Design	M_{nx}/Ω_b	$\phi_b M_{nx}$	M_{nx}/Ω_b	$\phi_b M_{nx}$	M_{nx}/Ω_b	$\phi_b M_{nx}$
Available Compressive Strength, kips							Available Flexural Strength, kip-ft					
ASD	LRFD	ASD	LRFD	ASD	LRFD		ASD	LRFD	ASD	LRFD	ASD	LRFD
109	1440	871	1310	793	1190		13.2	48.5	13.5	45.3	15.1	42.5
Available Strength in Tensile Yielding, kips						Properties						
P_n/Ω_t	$\phi_t P_n$	P_n/Ω_t	$\phi_t P_n$	P_n/Ω_t	$\phi_t P_n$	Limiting Unbraced Lengths, ft						
958	1440	871	1310	793	1190	L_p	L_r	L_p	L_r	L_p	L_r	
						13.2	48.5	13.5	45.3	15.1	42.5	
Available Strength in Tensile Rupture ($A_e = 0.75A_g$), kips						Area, in. ²						
P_n/Ω_t	$\phi_t P_n$	P_n/Ω_t	$\phi_t P_n$	P_n/Ω_t	$\phi_t P_n$	32.0 29.1 26.5						
780	1170	709	1060	647	970	Moment of Inertia, in. ⁴						
Available Strength in Shear, kips						I_x	I_y	I_x	I_y	I_x	I_y	
V_n/Ω_v	$\phi_v V_n$	V_n/Ω_v	$\phi_v V_n$	V_n/Ω_v	$\phi_v V_n$	1240	447	1110	402	999	362	
150	225	138	207	123	185	r_x , in.						
Available Strength in Flexure about Y-Y Axis, kip-ft						3.73		3.71		3.70		
M_{ny}/Ω_b	$\phi_b M_{ny}$	M_{ny}/Ω_b	$\phi_b M_{ny}$	M_{ny}/Ω_b	$\phi_b M_{ny}$	r_x/r_y						
231	348	207	311	181	273	1.67		1.66		1.66		

[†] Shape exceeds compact limit for flexure with $F_y = 50$ ksi.

[†] Shape exceeds compact limit for flexure with $F_y = 50$ ksi.





Example—Table 6-2

Given: W14x99, ASTM A992, pinned ends ($K = 1.0$),

$$L_{cx} = L_{cy} = L_b = 14 \text{ ft}$$

Check shape for combined loading using LRFD, with required strengths as follows:

LRFD
$P_u = 400 \text{ kips}$ $M_{ux} = 250 \text{ kip-ft}$ $M_{uy} = 80.0 \text{ kip-ft}$

79



Example—Table 6-2

Solution:

$$\frac{P_u}{P_c} = \frac{400 \text{ kips}}{1130 \text{ kips}} = 0.354$$

Because $\frac{P_u}{P_c} \geq 0.2$, use Spec. Eq. H1-1a:

$$\frac{P_r}{P_c} + \frac{8}{9} \left(\frac{M_{rx}}{M_{cx}} + \frac{M_{ry}}{M_{cy}} \right) \leq 1.0$$

$$\frac{400 \text{ kips}}{1130 \text{ kips}} + \frac{8}{9} \left(\frac{250 \text{ kip-ft}}{642 \text{ kip-ft}} + \frac{80.0 \text{ kip-ft}}{311 \text{ kip-ft}} \right) = 0.928 < 1.0 \quad \text{o.k.}$$

80



Table 10 - 1

14th
Ed.

15th
Ed.

Beam		Table 10-1 All-Bolted Double-Angle Connections												$\frac{3}{4}$ -in. Bolts		
Angle		$F_y = 50$ ksi $F_u = 65$ ksi														
		$F_y = 36$ ksi $F_u = 58$ ksi														
Bolt and Angle Available Strength, kips																
12 Rows		Bolt Group	Thread Cond.	Hole Type	Angle Thickness, in.											
					$\frac{1}{4}$		$\frac{3}{8}$		$\frac{1}{2}$		$\frac{3}{4}$		$\frac{1}{2}$			
W44		Group A	N	STD	197	295	246	369	286	430	286	430	361	541		
				ASD	197	295	246	369	286	430	361	541				
				LRFD	152	228	152	228	152	228	152	228				
				STD	129	194	129	194	129	194	129	194				
				ASD	129	194	129	194	129	194	129	194				
			LRFD	102	152	102	152	102	152	102	152					
			SSLT	197	295	246	369	286	430	361	541					
			ASD	196	294	216	323	216	323	216	323					
			LRFD	195	293	244	366	253	380	281	540					
			SSLT	197	295	246	369	286	430	361	541					
		ASD	196	294	216	323	216	323	216	323						
		LRFD	195	293	244	366	253	380	281	540						
		X	STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
			LRFD	152	228	152	228	152	228	152	228					
			STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
		SC Class A	STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
			LRFD	152	228	152	228	152	228	152	228					
			STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
		SC Class B	STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
			LRFD	152	228	152	228	152	228	152	228					
			STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
		SC Class C	STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
			LRFD	152	228	152	228	152	228	152	228					
			STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
		SSLT	STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
			LRFD	152	228	152	228	152	228	152	228					
			STD	197	295	246	369	286	430	361	541					
			ASD	197	295	246	369	286	430	361	541					
Beam Web Available Strength per Inch Thickness, kips/in.																
Hole Type		STD				OVS				SSLT						
		L_{wh} , in.				L_{wh} , in.				L_{wh} , in.						
L_{wh} , in.		$\frac{1}{2}$		$\frac{3}{8}$		$\frac{1}{2}$		$\frac{3}{8}$		$\frac{1}{2}$		$\frac{3}{8}$				
		ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD			
Coped at Top Flange Only		$\frac{1}{4}$	702	767	506	739	468	702	477	714	495	743	503	755		
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{3}{4}$	503	754	529	783	477	714	495	743	503	755	782			
		$\frac{1}{2}$	503	754	529	783	477	714	495	743	503	755	78			

Part 10. Design of Simple Shear Connections

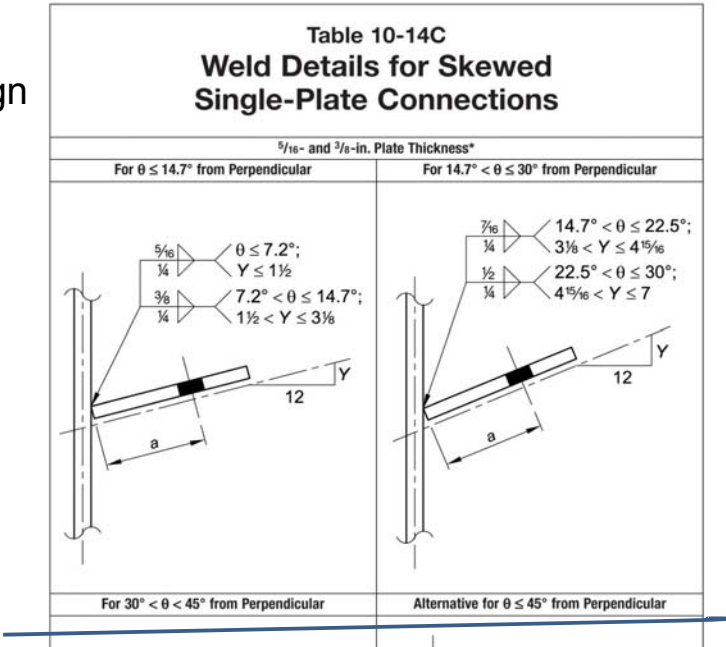


- Table 10-1 revised
- Single-plate connections: Stabilizer plate requirement
- Table 10-14C: Weld details for skewed single-plate connections

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Part 10. Design of Simple Shear Connections

- This is “One acceptable design aid for skewed welds....”
- Works for 36- or 50-ksi plates
- Added 5/8-in. plate



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Part 14. Design of Beam Bearing Plates, Column Base Plates, Anchor Rods and Column Splices



Table 14-2
Recommended Sizes for Washers and
Anchor Rod Holes in Base Plates

14th Ed:
3 1/2
4

14th Ed:
3

14th Ed:
1 13/16
2 1/16

Anchor Rod Diameter	Hole Diameter	Washer Size	Min. Washer Thickness	Anchor Rod Diameter	Hole Diameter	Washer Size	Min. Washer Thickness
in.	in.	in.	in.	in.	in.	in.	in.
3/4	1 5/16	2	1/4	1 1/2	2 3/8	4	1/2
7/8	1 9/16	2 1/2	5/16	1 3/4	2 7/8	4 1/2	5/8
1	1 7/8	3	3/8	2	3 1/4	5	3/4
1 1/4	2 1/8	3 1/2	1/2	2 1/2	3 3/4	5 1/2	7/8

14th Ed:
2 5/16
2 3/4

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Part 14. Design of Beam Bearing Plates, Column Base Plates, Anchor Rods and Column Splices



Table 14-2 Notes:

- 1. Hole sizes provided are based on anchor rod size and correlate with ACI 117 (ACI, 2010).
- ...
- 4. ASTM F844 washers are permitted instead of plate washers when hole clearances are limited to 5/16 in. for rod diameters up to 1 in., 1/2 in. for rod diameters over 1 in. up to 2 in., and 1 in. for rod diameters over 2 in. This exception should not be used unless the general contractor has agreed to meet smaller tolerances for anchor rod placement than those permitted in ACI 117.

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In Summary



- Part 1...New shape sizes and detailing dimensions
- Part 2...ASTM A500 Grade C is preferred for HSS
- Part 3...New footnotes
- Part 4...W-Shape column tables for 65 and 70 ksi
- Part 6...New Super Table 6-2
- Part 7...Table 7-14 includes TC bolts dimensions
- Part 8...New plastic method for eccentrically loaded bolt groups
- Part 9...Increased permitted tributary length for prying
- Part 10...Removal of stabilizer plate provisions
- Part 13...Additional considerations for HSS-to-HSS truss connections
- Part 14...Updated Table 14-2 for improved anchor-rod installation

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Design Examples V15.0



- Part I: Examples based upon the AISC Specification
 - Design of Tension Members
 - Design of Compression Members
 - Etc.
- Part II: Examples based upon the AISC Steel Construction Manual
 - Simple Shear Connections
 - Fully Restrained Moment Connections
 - Etc.
- Part III: System Design Examples
 - Design of Selected Four Story Building Members

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Design Examples V15.0

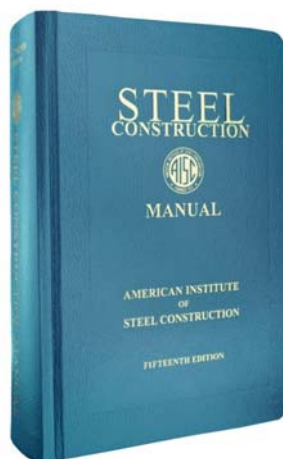


Part IV: Additional Resources

- Combined Flexure and Axial Force, W-shapes
(Table 6-1, 14th Ed. Manual)
- Filled HSS Column Tables, A500 Gr. C
(Tables 4-13 to 4-20, 14th Ed. Manual)
- New Super Table 6-2: W-Shapes, 65 and 70 ksi
 HSS, ASTM A1085
 HSS, A500 Gr. C
 Pipe
- New Z_{net} Table for Coped W-shapes

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Polling Question



Which of the following is NOT new to the 15th Edition Manual and 2016 standards?

- a. W-shape column tables for 65 + 70ksi
- b. Complete change to AESS provisions
- c. Increased hole size for all bolts
- d. Effective length is now L_c , not KL
- e. Larger HSS sizes added to Manual

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